Serial No. 40 GENERAL INFORMATION INCLUDING DESCRIPTIONS AND TESTS OF ELECTRIC AUXILIARIES TORPEDO BOAT DESTROYER No. 69 U. S. S. CALDWELL INFORMATION RELATIVE TO ITEMS UNDER THE COGNIZANCE OF THE BUREAU OF CONSTRUCTION AND REPAIR NAVY DEPARTMENT



Serial No. 40

GENERAL INFORMATION

INCLUDING

DESCRIPTION AND TESTS OF ELECTRIC AUXILIARIES

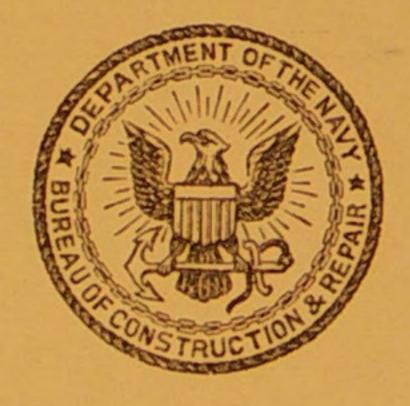
TORPEDO BOAT DESTROYER No. 69

U. S. S. CALDWELL

Information relative to items under cognizance of Bureau of Construction and Repair Navy Department

OFFICE OF CONSTRUCTION OFFICER FOR U. S. NAVY MARE ISLAND NAVY YARD, VALLEJO, CAL.

> Finished Plan No. 41 1917



WASHINGTON GOVERNMENT PRINTING OFFICE 1919

NATIONAL ARCHIVES FILES 50649

U. S. S. "CALDWELL."

CHRONOLOGY OF BUILDING.

Authorized by act of Congress The building assigned to Mare Island Navy Yard The date of completion to be Contract time Contract price First hull material ordered First large casting received Keel laid First frame raised First compartment tested Vessel launched Christened by First sea trial Standardization trials Speed trial, full power Inspected by board of inspectors Commissioned	October 30, 1915. January 1, 1918. 17 months. \$809,423. September 28, 1915. March 17, 1917. December 8, 1916. December 11, 1916. April 30, 1917. July 10, 1917. Miss Charlotte Caldwell. December 20, 1917. December 21–23, 1917. None held. December 14–20, 1917.
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This book was prepared by authority of the Bureau of Construction and Repair, and contains lists and description of various features and systems that have been installed under cognizance of that Bureau.

GENERAL INFORMATION.

LIST OF PLANS.

Furnished under the cognizance of the Bureau of Construction and Repair for ship use.

All of the following plans are a part of the ship's regular allowance of articles under cognizance of the Bureau of Construction and Repair, Equipage, Title "B," class 35.

Additional copies of any plan specified in this list may be issued to the commanding officer at his request for use on board ship. The booklet sets are issued to the commanding officer in sufficient number to provide one copy for each officer in charge of a department or division.

All plans issued to the vessel shall be receipted for, and shall be considered as a charge on the books of the executive officer under the same regulation as governing articles of equipage. All plans and booklets are to be considered as confidential documents.

METHOD OF MAKING UP FINISHED PLANS FOR PORTFOLIOS.

The plans furnished the vessel are in portfolios, 32 by 15 inches, bound on the 32-inch edge. The prints are taken on 30-inch wide blue-print paper, folded "bellows fashion," 13 inches wide, arranged so that the top fold presents the title of the plan without unfolding.

The inside front cover of the portfolio carries a list of plan numbers and a list of portfolio

numbers and titles of the plans.

An additional copy of the lists, inside the front cover of the portfolio, is made up into

booklet form for use in finding plans, and is left loose in the front part of the portfolio.

Blue prints of electrical auxiliaries, steering engine, windlass, etc., obtained from outside sources, are of miscellaneous sizes. They are attached together and folded as one set, and

the set assigned a single number in series of portfolio numbers.

There is one copy furnished of all the plans named in the list, except Booklets of General

Information and Booklets of General Plans, of which one copy is furnished for each officer.

Booklet of General Information and Final Inclining Experiment are not included with the plans made up in the portfolio; there is included, however, in the portfolio an uncut print of small-scale booklet plans of the vessel.

STATEROOMS AND BERTHS.

Commanding officer's stateroom and berth 1	
Wardroom, staterooms, and berths 5	
Chief petty officers' berths 10	
Chief petty officers' berths 10 Yeoman's office, berths 2	
Pilot house berths 2	
Radio room berth 1	
Crew's berths, forward 50	
Crew's berths, aft 32	
Total 108	

GENERAL DIMENSIONS.

Length over all Length between perpendiculars (8' $0\frac{1}{2}$ '' W. L.) 310' 0''. Breadth, molded (on 8' $0\frac{1}{2}$ '' W. L.) 30' 7''. Depth, molded at side (frame No. 88) 19' $8\frac{\pi}{8}$ ''. Tons per inch (7' $9\frac{\pi}{4}$ '' W. L.) 14.68 tons. Displacement (designed normal, 7' $9\frac{\pi}{4}$ '' W. L.) 15splacement (actual full load) Area of immersed middle line section Area of midship section (7' $9\frac{\pi}{4}$ '' W. L.) 404 square feet. Wetted surface (7' $9\frac{\pi}{4}$ '' W. L.) 50.597. 60.510. 60.597. 60.616icent prismatic 60.6496. 60.649	T1	0171 0111
Breadth, molded (on 8' $0_2^{1''}$ W. L.) 30' 7''. Depth, molded at side (frame No. 88) 19' $8_3^{2''}$. Tons per inch (7' $9_4^{3''}$ W. L.) 14.68 tons. Displacement (designed normal, 7' $9_4^{3''}$ W. L.) 1,080 tons. Displacement (actual normal) Displacement (actual full load) Area of immersed middle line section Area of water line (7' $9_4^{3''}$ W. L.) 204 square feet. Area of water line (7' $9_4^{3''}$ W. L.) 6,150 square feet. Wetted surface (7' $9_4^{3''}$ W. L.) 9,460 square feet. Wetted surface, full load Coefficient prismatic 0.597. Coefficient midship 0.597. Coefficient water line (designed 7' $9_4^{3''}$ W. L.) 0.6496. Area of rudder 68.14 square feet. Center of buoyancy (7' $9_4^{3''}$ W. L.) above base line 4' $6_4^{3''}$. Center of buoyancy (7' $9_4^{3''}$ W. L.) forward of middle perpendicular 0.04 foot. Transverse metacenter above center of buoyancy (7' $9_4^{3''}$ W. L.) 8' $8_4^{3''}$. Longitudinal metacenter above center of buoyancy (7' $9_4^{3''}$ W. L.) 8' $8_4^{3''}$. Center of gravity of water line (7' $9_4^{3''}$ W. L.) abatt middle perpendicular Frame spacing 15.72 feet. Free board at stem above 7' $9_4^{3''}$ W. L. 12 abatt middle perpendicular Frame spacing 15.72 feet. Free board at stem above 7' $9_4^{3''}$ W. L. 15. 17' $7_5^{3''}$. Rake of foremast 15.72 feet. 17' $7_5^{3''}$. Rake of stacks 17' in 1 foot.	Length over all	$315' 6\frac{1}{4}''$.
Depth, molded at side (frame No. 88) 19′ 8_8^{7} ″. Tons per inch (7′ 9_3^{4} ″ W. L.) 14.68 tons. Displacement (designed normal, 7′ 9_3^{4} ″ W. L.) 1,080 tons. Displacement (actual normal) 1,080 tons. Displacement (actual full load) 1,080 tons. Displacement feet. Displacement (actual full load) 2,094 square feet. Displacement feet. Displacement (actual full load) 2,180 tons. Displacement feet. Displacement (actual full load) 2,180 tons. Displacement feet. Displaceme	Length between perpendiculars $(8' 0\frac{1}{2}'' W. L.)$	310' 0''.
Tons per inch $(7' 9_3^{3})''$ W. L.)	Breadth, molded (on $8' 0\frac{1}{2}'' W. L.$)	30' 7".
Tons per inch $(7' 9_3^{3}'' \text{ W. L.})$	Depth, molded at side (frame No. 88)	$19' \ 8\frac{7}{8}''$.
Displacement (designed normal, $7' 9_4^{3''}$ W. L.) Displacement (actual full load) Area of immersed middle line section. Area of midship section $(7' 9_4^{3''}$ W. L.) Area of water line $(7' 9_4^{3''}$ W. L.) Wetted surface $(7' 9_4^{3''}$ W. L.) Coefficient block Coefficient prismatic Coefficient water line (designed $7' 9_4^{3''}$ W. L.) Coefficient water line (designed $7' 9_4^{3''}$ W. L.) Coefficient of buoyancy $(7' 9_4^{3''}$ W. L.) above base line Center of buoyancy $(7' 9_4^{3''}$ W. L.) forward of middle perpendicular Transverse metacenter above center of buoyancy $(7' 9_4^{3''}$ W. L.) Center of gravity of water line $(7' 9_4^{3''}$ W. L.) abaft middle perpendicular Center of gravity of full load water line abaft middle perpendicular Free board at stem above $7' 9_4^{3''}$ W. L.) abaft middle perpendicular Free board at stem above $7' 9_4^{3''}$ W. L.) Rake of foremast Rake of stacks Rake of stacks Rake of mainmast	Tons per inch (7' 9\frac{3}{4}'' W. L.)	14.68 tons.
Displacement (actual normal). Displacement (actual full load) Area of immersed middle line section. Area of water line $(7' 9_4^{21}'' \text{W. L.})$. Area of water line $(7' 9_4^{31}'' \text{W. L.})$. Cetted surface $(7' 9_4^{31}'' \text{W. L.})$. Coefficient block. Coefficient prismatic. Coefficient midship. Coefficient water line (designed $7' 9_4^{31}'' \text{W. L.})$. Coefficient water line (designed $7' 9_4^{31}'' \text{W. L.})$. Coefficient of buoyancy $(7' 9_4^{31}'' \text{W. L.})$ above base line. Center of buoyancy $(7' 9_4^{31}'' \text{W. L.})$ above dominated for middle perpendicular. Center of buoyancy $(7' 9_4^{31}'' \text{W. L.})$ forward of middle perpendicular. Center of gravity of water line $(7' 9_4^{31}'' \text{W. L.})$ abaft middle perpendicular. Center of gravity of water line $(7' 9_4^{31}'' \text{W. L.})$ abaft middle perpendicular. Center of gravity of full load water line abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board at stem above $7' 9_4^{31}'' \text{W. L.}$ abaft middle perpendicular. Free board	Displacement (designed normal, 7' 9\frac{3}{4}" W. L.)	1.080 tons.
Displacement (actual full load) Area of immersed middle line section Area of midship section $(7' 9_4^{3''} \text{ W. L.})$ Area of water line $(7' 9_4^{3''} \text{ W. L.})$ Between the section of the secti	Displacement (actual normal)	
Area of immersed middle line section. Area of midship section $(7' 9_4^{3''} \text{ W. L.})$ Area of water line $(7' 9_4^{3''} \text{ W. L.})$ By 460 square feet. Wetted surface, full load Coefficient block Coefficient prismatic Coefficient water line (designed $7' 9_4^{3''} \text{ W. L.})$ Coefficient water line (designed $7' 9_4^{3''} \text{ W. L.})$ Coefficient water line (designed $7' 9_4^{3''} \text{ W. L.})$ Coefficient of buoyancy $(7' 9_4^{3''} \text{ W. L.})$ above base line Center of buoyancy $(7' 9_4^{3''} \text{ W. L.})$ forward of middle perpendicular Center of buoyancy $(7' 9_4^{3''} \text{ W. L.})$ forward of middle perpendicular Center of gravity of water line $(7' 9_4^{3''} \text{ W. L.})$ abaft middle perpendicular Center of gravity of water line $(7' 9_4^{3''} \text{ W. L.})$ abaft middle perpendicular Frame spacing Free board at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perpendicular Freeboard at stem above $7' 9_4^{3''} \text{ W. L.}$ abaft middle perp	Displacement (actual full load)	
Area of midship section (7' $9\frac{3}{4}$ " W. L.) Area of water line (7' $9\frac{3}{4}$ " W. L.) Wetted surface (7' $9\frac{3}{4}$ " W. L.) Wetted surface, full load Coefficient block Coefficient prismatic Coefficient midship Coefficient water line (designed 7' $9\frac{3}{4}$ " W. L.) Area of rudder Center of buoyancy (7' $9\frac{3}{4}$ " W. L.) above base line Center of buoyancy (7' $9\frac{3}{4}$ " W. L.) forward of middle perpendicular Transverse metacenter above center of buoyancy (7' $9\frac{3}{4}$ " W. L.) Center of gravity of water line (7' $9\frac{3}{4}$ " W. L.) abaft middle perpendicular Center of gravity of full load water line abaft middle perpendicular Frame spacing Free board at stem above 7' $9\frac{3}{4}$ " W. L. Freeboard at stem above 7' $9\frac{3}{4}$ " W. L. Rake of foremast Rake of stacks Rake of mainmast	Area of immersed middle line section	
Wetted surface $(7' \ 9_4^{2''} \ W. \ L.)$ $9,460 \ \text{square feet.}$ Wetted surface, full load $9,460 \ \text{square feet.}$ $9,460 \ \text{square feet.}$ Wetted surface, full load $9,460 \ \text{square feet.}$ $9,490 \ \text{square feet.}$ $9,490 \ \text{square feet.}$ $9,400 \ \text{square feet.}$	Area of midship section (7' 93" W. L.)	201 gazzara faat
Wetted surface, full load Coefficient block Coefficient prismatic Coefficient midship Coefficient water line (designed 7' 9_4^2 " W. L.) Area of rudder Center of buoyancy (7' 9_4^2 " W. L.) above base line Center of buoyancy (7' 9_4^2 " W. L.) forward of middle perpendicular Transverse metacenter above center of buoyancy (7' 9_4^2 " W. L.) Congitudinal metacenter above center of buoyancy (7' 9_4^2 " W. L.) Center of gravity of water line (7' 9_4^2 " W. L.) abaft middle perpendicular Center of gravity of full load water line abaft middle perpendicular Frame spacing Free board at stem above 7' 9_4^2 " W. L Rake of foremast Rake of foremast Rake of mainmast	Area of water line (7' 93'' W L)	6 150 gamero foot
Wetted surface, full load	Wetted surface (7' 93" W L)	0,150 square feet.
Coefficient prismatic 0.597. Coefficient midship 0.854. Coefficient water line (designed 7' 9_4^{3} " W. L.) 0.6496. Area of rudder 68.14 square feet. Center of buoyancy (7' 9_4^{3} " W. L.) above base line 4' 6_2^{1} ". Center of buoyancy (7' 9_4^{3} " W. L.) forward of middle perpendicular 0.04 foot. Transverse metacenter above center of buoyancy (7' 9_4^{3} " W. L.) 8' 8_4^{1} ". Longitudinal metacenter above center of buoyancy (7' 9_4^{3} " W. L.) 741 feet. Center of gravity of water line (7' 9_4^{3} " W. L.) abaft middle perpendicular 15.72 feet. Center of gravity of full load water line abaft middle perpendicular 17' 7_2^{1} ". Free board at stem above 7' 9_4^{3} " W. L. 17' 7_2^{1} ". Rake of foremast 8' 7_2^{1} " W. L. 17' 7_2^{1} ". Rake of stacks 7' in 1 foot.	Wetted surface full load	9,400 square feet.
Coefficient midship 0.597. Coefficient water line (designed 7' 9_4^{3} " W. L.) 0.6496. Area of rudder 68.14 square feet. Center of buoyancy (7' 9_4^{3} " W. L.) above base line 4' 6_2^{1} ". Center of buoyancy (7' 9_4^{3} " W. L.) forward of middle perpendicular 0.04 foot. Transverse metacenter above center of buoyancy (7' 9_4^{3} " W. L.) 8' 8_4^{4} ". Longitudinal metacenter above center of buoyancy (7' 9_4^{3} " W. L.) 741 feet. Center of gravity of water line (7' 9_4^{3} " W. L.) abaft middle perpendicular 15.72 feet. Center of gravity of full load water line abaft middle perpendicular 17' 7_8^{1} ". Free board at stem above 7' 9_4^{3} " W. L. 17' 7_8^{1} ". Rake of foremast 8' 7_8^{1} " w. L. 8' 7_8^{1} ". Rake of stacks 7' in 1 foot.	Coefficient block	
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Area of rudder	Coefficient midshin	0.597.
Center of buoyancy $(7' \ 9\frac{3}{4}" \ W. \ L.)$ above base line 4' $6\frac{1}{2}"$. Center of buoyancy $(7' \ 9\frac{3}{4}" \ W. \ L.)$ forward of middle perpendicular 0.04 foot. Transverse metacenter above center of buoyancy $(7' \ 9\frac{3}{4}" \ W. \ L.)$ 8' $8\frac{1}{4}"$. Longitudinal metacenter above center of buoyancy $(7' \ 9\frac{3}{4}" \ W. \ L.)$ 741 feet. Center of gravity of water line $(7' \ 9\frac{3}{4}" \ W. \ L.)$ abaft middle perpendicular 15.72 feet. Center of gravity of full load water line abaft middle perpendicular 15.72 feet. Frame spacing 21". Free board at stem above $7' \ 9\frac{3}{4}" \ W. \ L$ 17' $7\frac{1}{8}$ ". Rake of foremast 8' $7\frac{1}{8}$ " in 1 foot. Rake of mainmast $7''$ in 1 foot.	Coefficient water line (deciened 7/ 02// W T	0.854.
Center of buoyancy $(7' \ 9\frac{3}{4}" \ W. \ L.)$ above base line 4' $6\frac{1}{2}"$. Center of buoyancy $(7' \ 9\frac{3}{4}" \ W. \ L.)$ forward of middle perpendicular 0.04 foot. Transverse metacenter above center of buoyancy $(7' \ 9\frac{3}{4}" \ W. \ L.)$ 8' $8\frac{1}{4}"$. Longitudinal metacenter above center of buoyancy $(7' \ 9\frac{3}{4}" \ W. \ L.)$ 741 feet. Center of gravity of water line $(7' \ 9\frac{3}{4}" \ W. \ L.)$ abaft middle perpendicular 15.72 feet. Center of gravity of full load water line abaft middle perpendicular 15.72 feet. Frame spacing 21". Free board at stem above $7' \ 9\frac{3}{4}" \ W. \ L$ 17' $7\frac{1}{8}$ ". Rake of foremast 8' $7\frac{1}{8}$ " in 1 foot. Rake of mainmast $7''$ in 1 foot.	Area of midden	0.6496.
Center of buoyancy (7' $9\frac{3}{4}$ " W. L.) above base line 4' $6\frac{1}{2}$ ". Center of buoyancy (7' $9\frac{3}{4}$ " W. L.) forward of middle perpendicular 0.04 foot. Transverse metacenter above center of buoyancy (7' $9\frac{3}{4}$ " W. L.) 8' $8\frac{1}{4}$ ". Longitudinal metacenter above center of buoyancy (7' $9\frac{3}{4}$ " W. L.) 741 feet. Center of gravity of water line (7' $9\frac{3}{4}$ " W. L.) abaft middle perpendicular 15.72 feet. Center of gravity of full load water line abaft middle perpendicular 15.72 feet. Frame spacing 21". Freeboard at stem above 7' $9\frac{3}{4}$ " W. L. 17' $7\frac{1}{8}$ ". Rake of foremast 8' $7\frac{1}{8}$ " in 1 foot. Rake of mainmast 7 " in 1 foot.	zrica di lududi	60 11 garrana faat
Transverse metacenter above center of buoyancy (7' 9\frac{3}{4}'' \text{ W. L.}) \text{ of middle perpendicular 0.04 foot.} 8' 8\frac{1}{4}'' \text{ Longitudinal metacenter above center of buoyancy (7' 9\frac{3}{4}'' \text{ W. L.}) 741 feet.} \text{ Center of gravity of water line (7' 9\frac{3}{4}'' \text{ W. L.}) abaft middle perpendicular \text{ 15.72 feet.} Center of gravity of full load water line abaft middle perpendicular \text{ Trame spacing \q	Center of buoyancy (1 97 W. L.) above base line	1/ 61//
Longitudinal metacenter above center of buoyancy (7' 9\frac{3}{4}'' W. L.) 241 feet. Center of gravity of water line (7' 9\frac{3}{4}'' W. L.) abaft middle perpendicular 25.72 feet. Center of gravity of full load water line abaft middle perpendicular 21''. Free board at stem above 7' 9\frac{3}{4}'' W. L. Freeboard at stern above 7' 9\frac{3}{4}'' W. L. Rake of foremast 8' 7\frac{1}{8}''. Rake of stacks 7'' in 1 foot. Rake of mainmast 7'' in 1 foot.	out of buoyanty (1 97 W. L.) Torward of middle normandianter	O O1 foot
Center of gravity of water line (7' 9\frac{3}{4}'' W. L.) abaft middle perpendicular. Center of gravity of full load water line abaft middle perpendicular. Frame spacing. Free board at stem above 7' 9\frac{3}{4}'' W. L. Freeboard at stern above 7' 9\frac{3}{4}'' W. L. Rake of foremast. Rake of stacks. Rake of mainmast.	The state of the later above center of him vaner (7' 03') W	0/01//
Center of gravity of full load water line abaft middle perpendicular Frame spacing Free board at stem above 7' 9¾'' W. L Freeboard at stern above 7' 9¾'' W. L Rake of foremast Rake of stacks Rake of mainmast	The structure inconcentral above center of phovener (7' 03') W	711 foot
Frame spacing	COLUMN OF CITAL AND COLUMN OF THE COLUMN OF	C
Free board at stem above $7' 9\frac{3}{4}''$ W. L. Freeboard at stern above $7' 9\frac{3}{4}''$ W. L. Rake of foremast. Rake of stacks. Rake of mainmast. $\frac{7}{8}''$ in 1 foot.	District of the today water into another middle morning	
Freeboard at stern above 7' $9\frac{3}{4}$ " W. L. Rake of foremast. Rake of stacks. Rake of mainmast.	THE RESIDENCE OF THE PROPERTY	
Rake of foremast $\frac{8'}{7}$ in 1 foot. Rake of mainmast $\frac{7''}{8}$ in 1 foot.		1 - 1 1 1
Rake of stacks. Rake of mainmast	THE PARTY OF THE P	
Rake of mainmast in 1 foot.		Per 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		THE R P
Camber		
15" in 30 feet.	Camber	8 In 1 100t.
		15" in 30 feet.

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LOADS CONTEMPLATED IN DETERMINING THE MEAN DRAFT CORRESPONDING TO THE "DESIGNER'S WATER LINE."

In the design of the vessel the mean draft corresponding to the "designer's water line," viz, 7' 9\frac{3}{4}", contemplated the following condition of loading:

Ship complete, ready for service in every respect, with full complement of officers and crew and their effects, and consumable load, as tabulated below:

AMMUNITION, INCLUDING TORPEDOES, DETAILED AS FOLLOWS (FULL SUPPLY).

Quantity.	Pounds.	Tons.
	33, 500	14. 95
0 rounds 4"/50 caliber ammunition		2.09
and the section of th	~ ~ ~ ~	. 22
000 1 00 I-b on boll Model IMID	~ 1	. 037
and 1.00 caliban blonk Model 1909	0.0	. 029
and I on a labour darmony Model 1900	000	. 178
and 1, 90 calibox ball Model IX9X	7 -0	.074
200 - J- 20 calibon blank Model 1898	~~~	. 24
1 4 -1 b - 1 h - 1		2. 30
rounds warheads (not boxed)	5, 160	
rounds warneads (not boxed)	28, 680	12.80
rounds torpedoes	271	. 12
uperheaters, detonators, primers, etc		1. 33
applies and accounts stores (two-thirds supply)		6. 57
upplies and accounts stores (two-thirds suppry)		.00
avigation stores (two-thirds supply)		. 36
avigation stores (two-thirds supply)		1.66
Lance on other course of the c		
fficers' stores (two-thirds supply)		. 66
quipment stores (two-thirds supply) resh water (two-thirds supply)		9.90
resh water (two-thirds supply)		12. 33
CONTRACTOR (TITO) TO IT (IN CITO) TO IT (IN CI		
uel oil for galley range (two-thirds supply)		.06
uel oil for galley range (two-thirds supply)		.00

VOICE TUBES.

Voice tubes are installed to accomplish two general purposes, namely, general ship's service and fire control. Return electric calls with water-tight push buttons, bells, annunciators, etc., are installed in connection with general ship's service. The fire-control system is not provided with calling devices. The following table contains the principal data relative to points connected, size of tube, type of mouthpieces, etc.:

Voice tube No.	Diameter (inches).	From-	Type of mouthpiece.	То—	Type of mouthpiece.	With calls.	With- out calls.
1	2	Bridge at wheel		Pilot house at wheel	Meg		Y
2	3	Bridge and pilot house	2 N. W	Engine and auxiliary room	2 N. C	X	21
3	3	Bridge and chart house	1 N. C	}Wardroom	N. C	X	-
4	3	Engine room		Forward and after boiler		X	43.0
5	3	Bridge and pilot house	(1. IV. U	Captain's and second offi- cer's staterooms.	}	X	
6	3	Bridge and chart house	1 N. W	Radio room	N. C	X	
7		Bridge and pilot house	$\begin{cases} 1 \text{ N. W} \\ 1 \text{ N. C} \end{cases}$	After steering station and steering engine room.	}2 N. W	X	
x 8 x 9	3		41. 11	TOTO POLDEGO PHOES	2 spec	1	X
10	3	After steering station	N. W	Starboard torpedo tubes	2 spec		X
11	3	Engineer's stateroom	IV. VV	Engine room	N. C	X	
x 12	3	Bridge, starboard and port	2 N W	Antiaircraft gun No. 1	N. C	X	-
x 13	3	do	2 N W	Antiaircraft gun No. 2	W. T		X
14		wheels.		Master gyro compass	N. C	X	X
15	3	After steering station	N. W	Steering engine room		v	
x 16	3	4-inch rapid-fire gun No. 1	WT	Bridge and gional mlatform	2 N W	Λ	v
x 17	-	THE TRIPIC THE SUIT IN U. D.	VV	do	O AT TIT		A V
x 18		Tallou Incall Incall Inc	VV	MA .	2 N. W		A V
x 19	4	4-inch rapid-fire gun No. 4	(W. T	}do	(N. C)		A V
x 20	3	Forward spotter's ton	(N. C	,	[N. W]		Λ
x 21	3	Gun platform	N W	do			X
x 22	3	After spotter's top.	N. W	Top of deck housedo	N. W		X

In the above table the following abbreviations have been used for mouthpieces:

	- Lio deliprocob.	
Symbol.	Stands for—	In accordance with Plan No.—
Meg. W. T.	Megaphone mouthpiece W. T	C. and R. Plan No. 24403. C. and R. Plan No. 24403. S. E. Plan No. 1834L.

Voice tubes are seamless, 49 mils thick for a straight lead and 10.9 mils thick for bends. The tubes in general are run close up under the main deck on the port and star. side, and where necessary to pass them through the fuel-oil tanks are carried in a duct provided for the purpose. Deck and bulkhead stuffing tubes are used where tubes pass through decks and bulkheads. Single hangers for voice tubes are in accordance with Bureau of Construction and Repair's Plan No. 19642, and where a number of tubes are run together, a plate hanger having the required number of holes to support the group is used.

STEERING ARRANGEMENTS.

(See Plans Nos. 25-25A in portfolio.)

The steering gear is of the horizontal right and left hand screw type, single thread, the traveling nuts being connected to the rudder crosshead by links. A spur gear on the forward end of the screw gear meshes with a pinion on the crank shaft of the horizontal two-cylinder 7 by 7 inch screw gear, steam engine, located on the center line under the screw shaft. The engine and gear and also the wheels for hand operations are located in D-204, the aftmost compartment on the first platform deck.

The engine is provided with automatic follow-up type of control and is operated by wire rope transmission and shafting from the pilot house, bridge, and top of after deck house, and a trick wheel mounted on the center line of the engine. Clutches are provided to disconnect each wheel while the others are in use.

.....

..... X

W..... X

c.....

with Plan No.-

No. 24403. No. 24403.

1834L.

The rope transmissions are of $\frac{2}{3}$ -inch diameter plow-steel wire, wound on grooved drums, forward and aft. The lead from top of after deck house is run under the main deck, on the starboard side, in 1-inch brass pipes, standard ties with plugs being placed in the piping for lubricating the leads. The leads from the pilot house and bridge are led aft on top of the main deck, on the starboard side, fair leaders being provided in the sockets of awning and rail stanchions. The forward drum is mounted on a shaft, connected by miter gears, to the vertical shaft of pilot house and bridge steering stands, and located in the pilot house on the starboard side. The forward drum of after system is mounted on a shaft connected to the vertical shaft of after steering stand by miter gears and is hooked up under the top of after deck house on the center line. The after drums are mounted on a shaft and connected by a set of bevel gears to the vertical shaft of the engine valve-operating gear. A wrench is provided for turning drums in taking up slack of transmission leads.

To operate the screw gear by hand two 5-foot wheels are installed forward of the screw shaft and directly connected by means of a sliding clutch. When steering by hand the engine pinion is withdrawn by a clutch operated by a handwheel just forward of the pinion bearing.

An emergency spare tiller is permanently fitted over top of rudderstock, above the main deck, and operated by a relieving tackle of 3½-inch manila rope run continuously through 10-inch iron blocks attached to tiller and pad eyes at frame 174½.

INSTRUCTIONS FOR STEERING FROM THE VARIOUS STATIONS.

TO STEER BY STEAM FROM PILOT HOUSE.

Disconnect the clutch over steering stand in the pilot house and trick-wheel clutch on the vertical shaft on port side of steering engine, throw into forward position the clutch lever on the fore-and-aft drum shaft over the steering engine on port side; disconnect the hand-steering-wheel clutch at forward end of screw shaft, and connect the clutch on the forward side of engine spur gear.

TO STEER FROM BRIDGE BY STEAM.

Proceed as for "Steering from pilot house," except that the clutch over pilot-house stand is to be connected and pilot-house wheel disconnected.

TO STEER BY STEAM FROM AFTER DECK HOUSE.

Disconnect the trick-wheel and handwheel clutches as for "Steering from pilot house," and throw into aft position the clutch shifting lever on the fore-and-aft drum shaft over the steering engine on the port side.

TO STEER BY HAND FROM STEERING ENGINE ROOM.

Disconnect the engine spur-gear clutch and connect the clutch between the hand steering wheels and screw shaft.

STEERING GEAR DATA.

Builders: Lidgerwood Manufacturing Co., New York.		
Type: Horizontal screw gear, double-thread engine.		
37 1 6		2
Number of cylinders	menes	7
Charles of nictons	u0	1
Working steam pressure	pounds	200
Designed to withstand full boiler pressure	inches	200
Steam supply pipe, diameter	do	2
Steam exhaust pipe, diameter	degrang	25
Angle of steering engine stops	do	99
Angle of rudder stops. Revolutions of screw shafts from extreme right to extreme left.		10
Revolutions of screw sharts from extreme right to extreme left	Mark De Lotter Les Lotter	00
Revolutions of engine pinions, extreme right to extreme reconstructions of steering stand wheels, 70 degrees		12
Revolutions of steering stand wheels, 70 degrees		20.
Revolutions of handwheel, 70 degrees		44
Ratio of screw spur gear to engine pinion		5.
Lead of screw	inches	1
Depth of Acme thread	do	Will I
Radius of rudder crosshead	do	20
Diameter of rudderstock, outside		
Diameter of rudderstock, inside	do	5
Total area of rudder	square feet	68.
Area of balanced portion	do	10.

METHOD OF UNSHIPPING RUDDER.

Remove portable plate on main deck, disconnect steering gear links from crosshead, and remove the taper pin connecting the rudder frame and stock. By using a reverse-acting pin or drift in the slot, the rudderstock can be started loose from the frame.

ANCHOR HANDLING AND WINDLASS.

The anchor windlass is located on the main deck between frames 13-15 on the center line. It is operated by a vertical type steam engine mounted on the after side of bulkhead No. 12, between the first platform and main deck. The engine drives the windlass and wildcat through a vertical shaft, the transmission being through worm gearing.

The engine may be cleared from the vertical shafting by removing the toggle connecting the worm wheel to its rim. A locking head is located between the gypsy and wildcat and keyed to the vertical shaft. Block keys engage the locking head to the gypsy head and wildcat so that they can be operated together or separately.

For heaving by hand it is necessary to remove the block key connecting the worm wheel center to its rim below the main deck.

The windlass machinery was manufactured by the American Engineering Co., of Philadelphia. The engine is designed for a working pressure of 200 pounds per square inch, the specifications requiring that it be capable of withstanding the full boiler pressure of 265 pounds per square inch. The engine is a direct-acting, reverse-valve type, 5 by 5 inches, with two cylinders. It has a 1½-inch steam supply and 2-inch exhaust, and is controlled from the main deck by means of a handwheel, operating the throttle valve through a connecting rod and lever

The wildcat is designed to take a 1-inch United States Navy standard, close link, anchor chain, furnished by the Government. For controlling the wildcat a friction-band brake is fitted, which provides control for either direction of rotation, the gear consisting of two turn-buckle screws, operated by handwheels.

Riding bitts are fitted forward of the windlass and chain clearers so arranged as to clear the chain from the wildcat when running in either direction. Compressors are fitted under the main deck to compress the chain in the pipes with the use of purchase tackle. Deck stoppers are provided for holding chains, secured to deck pads, etc. A crane for handling the anchor on deck is mounted at the center line on main deck between frames 4 and 5. Tackle with purchase, secured to bitts on either port or starboard side between frames 18–20, is provided so that it can be hauled in by gypsy head.

AMMUNITION HANDLING AND LOADING ARRANGEMENTS.

The forward torpedo crane is located on the boat davit at frame 109, port, and the after torpedo crane is located on the boat davit between frames 130 and 131, and are used for handling torpedoes from the ship's side and transferring them to the trolley tracks, which extend from the forward to the after tubes on port and starboard sides. These tracks are I beam, attached to the underside of boat skid beams and are so located at ends as to support the torpedo while loading into tubes. Two trolleys are provided for use on these tracks and have all been tested to 5,600 pounds, which is twice the working load.

The torpedoes are normally stowed in the triple tubes, provision being made in the forward and after magazines, compartments A-112 M and D-105 M, for stowing of war heads. These war heads are handled in the magazines by purchases hooked into pad eyes, suitably located.

Two davits, tested to 1,000 pounds, are provided for striking down the ammunition and war heads to their stowage spaces.

LIST OF AMMUNITION STOWAGE.

1es .. 1

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khead No. 12, ildcat through

cle connecting I wildcat and

d and wildest

worm wheel

Type.	Compartment.	Total. capacity.	A llow- ance.	Number in each box or tank.	Length.	Width.	Depth or diameter.	Weight of each box or tank.
					Inches.	Inches.	Inches.	Pounds.
4 in. 50-caliber cartridge	A-111 M D-106 M	308 166	} 400	1	51.92		6.32 D	83.75
1-pounder antiaircraft	A-110 M	10	10	100	31.25	17	10.3	235
Do	D-106 M	10	10	100	31.25	17	10.3	235
War heads	A-112 M	6	6				21 D	430
Do	D-105 M	6	6				21 D	430
.45-caliber ball, 1911	A-110 M	5	1	2,000	16. 25	12.75	7.625	110
.30-caliber dummy, 1906	A-110 M	1	1	1,000	21.625	12.5	7.0	66
.30-caliber blank, 1909		1	1	2,000	17. 125	12.45	11.75	84
.30-caliber ball, 1898		4	2	1, 200	34.5	9	7.5	99.75
.30-caliber ball, 1906, for rifle		5	17	800	34.5	9.5	8. 25	100
.30-caliber ball, 1906, for machine gun.		20	30	800	34.5	9.5	8.25	100
.30-caliber blank, 1898	1	4	2	1,000	19.75	13.125	8.0	44.5
Torpedo detonator	1	6	6	4	43	338	33	2
Impulse primer		6	6	24				2.5
Superheater fuses	1 440 45	7	7	20		018	7 9	3
Net cutters	1	3	3	4	$32\frac{1}{2}$	$9\frac{13}{16}$	$7\frac{9}{32}$	55
Impulse powder	A-110 M	1	1	50				58

BATTERY.

	Loc	Location.				
Caliber.	Deck.	Frame.	Gun No.			
GUNS.						
4-inch rapid-fire gun	Main	29, center line	al :			
ANTIAIRCRAFT. 1 pounder automatic	Main	port				
6.8 M by 21 inches triple Do		. 107, starboard				

SMALL ARMS.

a liber	Location.	Stowed in—
.45 caliber Colt's revolver	Small-arms magazine A-110 M	Racks. Boxes.

Stowage is also provided on deck for the above-mentioned small arms.

BOATS.

Number.	Name.	Carrying capacity.
	24-foot motor sailing launch 24-foot whaleboat 21-foot motor dory 14-foot wherry 10-foot punt 7 foot 6 inch by 3 foot 6 inch life rafts (cylinder).	19 men. 23 men. 10 men. 5 men. 14 men each.

SEA VALVES.

				201 (1		
Size and type.	Compart- ment.	Name.	Frames.	Side.	Bureau.	Service.
2½-inch special globe	B-101	Boiler room	57-58 58-59		S. E S. E	Evaporator blow. Ice-machine discharge.
14-inch special angle	B-101 B-101	do	67-68		S. E	Fire and bilge pump suction.
3½-inch special cross	В-101	do	69–70	P	S. E	Fire and bilge pump discharge.
3-inch special angle	В-102	do	88-89	P	S. E	Fire and bilge pump suction.
3½-inch special cross	В-102	do	89–90	P	S. E	charge.
1½-inch special globe	В-102	do	94–95	S		suction.
Do	В-102	do	95–96	S	S. E	discharge.
20-inch special gate	C-102	Engine room	101–105	P. and S.	S. E	1.41.0
4-inch special angle	C-102	do	117-118	P	S. E	pump suction. Oil-cooler circulating
3½-inch special angle	C-102		119–120	P.and	S. E	pump discharge.
20-inch special gate	C-102	Auxiliary room.		S		Janaar and
			125-126	Q	SE	tion. Air and circulating pump
Do	. C-103	do	The state of the s	HELE	D. E	discharge.
2-inch special angle	. C-103	do	126–127 126–127		S. E S. E	Fire and bilge pump and
4-inch special angle	. C-103	do	127-128	P	. S. E	Fire and bilge and evapora- tor feed suction.
	No. of the last	The state of the s	The second		A COLUMN TO SERVICE	

CRA OPENINGS BE

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9 inches
12 inches
12 inches
13 inch

strong pump suction... 3 including pump discharge. 6 including pump discharge. On A may and circulating 11 in 11 in 12 i

mp discharge...... 84 inc.
6 inch
and evaporator feed 11 inc

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tend into fuel-oil tanks, where black and into fuel-oil tanks, where black using takes in fuel-oil tanks are persent the whole length of the pipe who have are of mild steel, galvant are of brass.

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and not has 35 feet of nine-thread residence and not has 35 feet of nine-thread residence and not have a see wrought steel when the holds are wrought steel when the holds are water the bolts a seminate with bilge water the bolts a seminate with bilge water the bolts a seminate in mallea water and gate valves is accomplishing and deck plates may be added to the seminate and deck plates may be added to the seminate in mallea.

SOUNDING TUE

In compart ment—

A-302.

A-302.

MACHINERY.

ENGINES.

The vessel is fitted with a two-shaft arrangement of General Electric Co.'s turbines with reduction gear, placed in one common water-tight compartment and arranged as follows:

Starboard shaft, driven through gearing by one main turbine and one cruising turbine, the connection between the main turbine and the cruising turbine being accomplished by electrical means through a speed-reducing clutch.

Port shaft, same as starboard.

The main turbines are fitted with stages for running astern and the backing turbines are capable of developing not less than 25 per cent of the horsepower required to obtain the full speed ahead.

The reduction gears are located directly aft of the main turbines.

For "full speed" steam is admitted into the third stage of each main turbine.

For "high cruising speed" steam is admitted into the first stage of the main turbines.

For "low cruising speed" steam is admitted into the cruising turbines and then into the main turbines.

PROPELLERS AND SHAFTS.			
Diameter of propeller shafting	inches	101	
Diameter of line shafting	aoaoa	101	
Diameter of axial hole in shafting	do	$6\frac{3}{4}$	
Number of propellers		2	
Number of blades each propeller (cast solid)		3	
Diameter of propellers (designed)	inches	97	
Pitch of propellers fixed (designed)		105	
Ratio of diameter to pitch (designed)		1. 082	
Area, projected (designed) D	square inches	4, 213	
Area, helicodial (designed)		H 200 0	
Area, disk (designed)	square inches	7, 389. 8	
Lower tip of blade below bottom of keel	inches	1116	
Tips of blades below 7 feet 93 inches water line	do	20.5	
Material of propellers, manganese bronze.			
Starboard propeller is right hand.			
Port propeller is left hand.			

BOILERS.

Kind of boiler (oil burning), Thornycroft water boiler.	
Number (two in each boiler room)	4
Designed working pressurepoundspounds	265
Heating surface, each boilersquare feetsquare feet	5, 984
Cubical contents of combustion chamber, each boilercubic feet	600.56
Diameter of main steam pipesinches	91/2
Diameter of steam pipe, for each boiler	7
Number of off burners, each boiler	9
rumber of furnaces, each boller	1
MINURU DIDOS, HEIVID MINUVA DUCA DIVA (MANTALA)	46' 5"
Number of smoke pipes	4
Area of section through each pipe	17.1
Oil fuel system is of Bureau of Steam Engineering mechanical atomization type, with	
Number of smoke pipes. Area of section through each pipe. Oil fuel system is of Bureau of Steam Engineering mechanical atomization type, with Bureau of Steam Engineering standard air controlling registers and burners.	
8 - The Controlling registers and burners.	

ELECTRIC PLANT.

GENERATORS.

Electricity for lighting the ship, for the three ventilating sets, and for all other uses on the vessel, is furnished by two 25-kilowatt, 125-volt, continuous-current turbo-generators, supplied by the Westinghouse Electric Co.; each generator is mounted on a common bedplate and direct connected to a horizontal steam turbine.

The generator and distribution switchboards are combined in one frame and are located on the end of dynamo flat in auxiliary room.

WIRING, ETC.

The two-wire system of distribution is employed. It is designed on the basis of allowing a maximum drop in potential of $2\frac{1}{2}$ per cent for lighting and 5 per cent for power feeders from the generator bus bars to the farthest lamp or motor on a circuit.

The wiring throughout the ship is Navy standard leaded and armored wire. This is installed and arranged to interfere as little as possible with other devices and appliances on

the vessel and with due regard to the ship's structure.

Where wires pass through decks, bulkheads, etc., they are provided with approved stuffing tubes and fittings, and where water-tightness is required these devices are water-tight.

The location of each auxiliary and the leads of all feeders are shown on finished plan No. 18055, which is a combined plan of the power and lighting leads. Prints of this plan have been furnished the ship.

LIGHTING AND POWER LEADS.

Feeder No.	Character of service.	Rated amperage, full load.	Wire size, C. M.
B-1 B-2 B-3 L-4 L-5 B-7 B-8 P-9 P-11 P-13 P-14	Battle lighting, forward Battle lighting, aft. Engine and boiler rooms. General lighting, aft. General lighting, forward Searchlight, forward Searchlight, aft. Tools and refrigerator box Radio room Vent motor, forward. Vent motors, aft.		18,000 C. M. T. C. 30,000 C. M. T. C. 30,000 C. M. T. C. 37,000 C. M. T. C. 2—100,000 C. M. S. C. 2—100,000 C. M. S. C. 40,000 C. M. T. C. 60,000 C. M. T. C. 18,000 C. M. T. C.

SEARCHLIGHTS.

Search- light No.	Size.	Located on—	Operated—
1 2	30-inch	Searchlight platform on bridge	On bridge. On aft deck house.

GENERAL DIRECTIONS FOR THE MAINTENANCE AND REPAIR OF ELECTRICAL APPLIANCES ON SHIPBOARD.

GENERAL.

The life and satisfactory operation of all electrical apparatus is dependent on proper care as well as the original design of the appliance. It is therefore strongly recommended that such apparatus receive frequent and careful inspection and prompt correction of any defects or faults which may develop.

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het are frequently and are not loose; he hat they for the hat no fore he had been on the he had he commutate him the com

CLEANLINESS IS ESSENTIAL.

Always keep every piece of electrical apparatus clean and free from all dust, oil, and moisture, especially the windings of motors, solenoid coils, etc., also all rheostats.

Care should be taken when operating switches, controllers, and starting arms of control panels to see that no arcing or burning of the contacts takes place. Open field switches, when they are provided, slowly, allowing the field to discharge through the drawn-out spark thus formed. This method of opening the field circuit avoids excessive potential in the field coils which might break down the insulation.

A breakdown of the insulation on any piece of electrical apparatus may result in abnormal currents and overheating. It is also possible for a high resistance path to be formed by coal dust, salt moisture, carbon dust from the brushes, or oil, which would cause overheating or a breakdown of the insulation.

If moisture is detected in any piece of electrical apparatus, a test for insulation resistance should be made immediately, and any defect or fault found should be corrected at once if it is possible to do so on board ship.

A convenient means of drying out a piece of electrical apparatus when it can not be removed to a drying room is to pass a reduced current (say from one-fourth to one-half normal) through the part affected; a lamp bank or a water rheostat in series with an ammeter may be used for this purpose. The current may be gradually increased to normal load if no trouble or defect occurs, and should be left on enough to insure a thorough drying out of the appliance. Fuses of suitable size should always be inserted in the circuit when drying out apparatus by this method.

MOTORS.

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F ELECTRICAL APPLIANCE

us is dependent.

re strongly recommended

The following general suggestions relate to the proper care and dismantling of motors:

YOKE.

If for any reason a brush yoke is to be removed, the yoke, the casting to which it fits, and all connections should be plainly marked so that they may be readily replaced in their original positions. The proper position of the yoke is determined when the motor is tested at the factory and should be plainly marked. However, as these marks correspond to the full-load position, and as the motor may run at less than full load, it may be necessary to shift the position of the brushes slightly to secure the best commutation.

STUDS.

One of the most common sources of trouble in a motor is the breaking down of the brush holder stud insulation, causing grounds and short circuits. Careful inspection and a thorough cleaning off from the brush rigging, especially at the insulated points, of any dust or oil that may accumulate, will lessen the liability of trouble from this source. A stud bushing or washer saturated with oil should be replaced by a new one.

In fitting new insulation to brush holder studs particular attention should be given that each stud has the same relative position in the yoke and that the distance from all studs to the commutator is uniform.

These are frequently a source of trouble; examine them regularly and be sure that the connections are not loose; that they have the proper pressure on the commutator and are properly spaced; also that they fit the commutator perfectly and are free to move up and down in the holders, and that no foreign substance is caught between a brush and the commutator.

BRUSHES.

The tension on the brushes should be kept as nearly uniform as possible and should approximate 2 pounds per square inch of brush-contact area. The pressure may be adjusted by a small spring balance, which can be attached to the end of the brush spring, and then pulling the balance away from the commutator in line with the axis of the brush for about ½ inch.

On bipolar motors the brushes should be set diametrically opposite and on multipolar machines brushes of like polarity should be opposite, except on such multipolar machines which, due to their construction, do not have the same number of brush studs as poles. In machines of the latter type the spacing between brushes of opposite polarity should be the same.